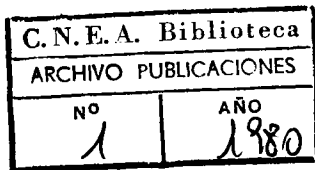


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Neutron thermalization process in benzene¹

Die Thermalisierung von Neutronen in Benzol

By Maximo J. Abbate, José V. Lolich and H. Wio*

Introduction

The close relation between the molecular dynamics of the moderators and the neutron thermalization process in them is widely known.

Since these processes have fundamental importance in the design of thermal nuclear power plants there is interest to obtain a precise description and knowledge about them.

The problem so explained is highly complex in a general point of view because firstly implies to formulate particular models for each molecular species that can be found in the reactor, and secondly the definition of these models is limited to semiempirical procedures, that means the models are not totally independent from the experimental information that they intend to reproduce with its results. To consider different moderators we selected and studied primarily the H₂O and D₂O, and then we included too the benzene in order to analyze a fairly complex molecular structure but with symmetrical properties sufficient to simplify the problem.

So, a new and general scheme for the description of the molecular dynamics was applied to this material [1] and the available experimental information about neutron total cross section and diffusion parameters was completed [2]. At this point, three different models based in other known vibrational frequency spectra were used and the scattering laws obtained with them showed better agreement than earlier models.

In this paper we present an additional test on the cited calculational scheme consistent with differential neutron spectra measurements in a clean geometry and its comparison with results from the transport theory.

Description of the experiments

The experimental facilities and procedure used in this work were detailed fully in Refs. [3] and [4].

The principal part of the experiment was the measurement of the angular neutron spectra as a function of the position in pure C₆H₆ at 23°C using the time-of-flight technique. The experimental arrangement is shown in Fig. 1

A 30 × 30 × 50 cm³ assembly lined with a cadmium sheet and shielded with a boron mixture was used. The neutron beam was extracted via a 25 mm diameter reentrant hole.

Static measurements of the thermal and epithermal flux distributions were made using indium foils in conjunction with the cadmium difference method. From the epithermal flux distribution in the reentrant hole direction, the spatial form of the moderation source was obtained and from the distribution perpendicular to this,

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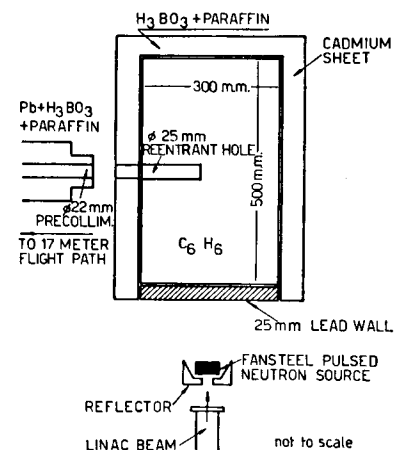


Fig. 1: Experimental arrangement

the inverse relaxation constant, γ , was derived to get the local buckling, the results were:

$$\begin{aligned} \gamma &= 0,181 \text{ cm}^{-1} (\pm 5\%) \\ \text{Total } B^2 &= -0,0121 \text{ cm}^{-2} \\ \text{Transverse } B^2 &= -0,0224 \text{ cm}^{-2} \end{aligned}$$

and the thermal leakage term was:

$$DB^2 = -0,00454 \text{ cm}^{-1}$$

Through the measurement of the thermal neutron decay constant ($\alpha = 4220 \pm 20 \text{ sec}^{-1}$) and an auxiliary calculation performed with the NYR261 Code [5] the mean emission time necessary for the experimental data correction was obtained.

A neutron spectrum was measured in the middle of the assembly, and the leakage spectrum too, and to complete prior study performed in H₂O related to interfaces with vacuum [6]. The measured spectra are shown in Figs. 2 and 3. In order to perform the correct background subtraction (using a B-10 filter) the neutron beam intensity was monitored with two U-235 miniature fission counters located inside the vessel. The responses of these detectors agreed within 1% during all measurements. In all cases the standard deviation due to statistics was less than 4% over all the energy range. The correction derived from the time resolution function was less than 1%. The data reduction was made with the NYRTOF Code [7], the poorest energy resolution was 9%, and outside the energy range from 0.07 to 0.24 eV was better than 5%.

Theoretical calculations

Molecular Models

In order to obtain the group cross sections to be used in the transport calculations the first problem was to select the molecular model. Known models were considered [8–11], and can be reached the conclusion that it was convenient to develop a new theoretical scheme able to represent the complex molecular system dynamics [1].

This scheme gives a kind of global description of the dynamics of complex and polyatomic systems through adequate frequency spectrum and effective masses and reduces the diversity and quantity of calculations necessary to obtain the molecular scattering law from codes of the GASKET type [12].

The first results obtained with this scheme were described in [1], and mean that it is possible to reach better agreement with the experimental scattering law for

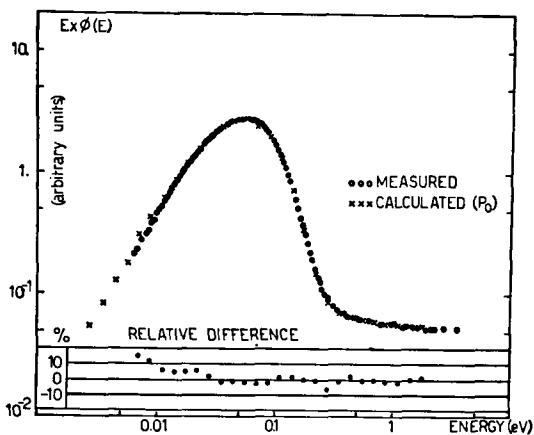


Fig. 2: Measured central neutron spectrum in C_6H_6 compared to calculation using P_0 approximation

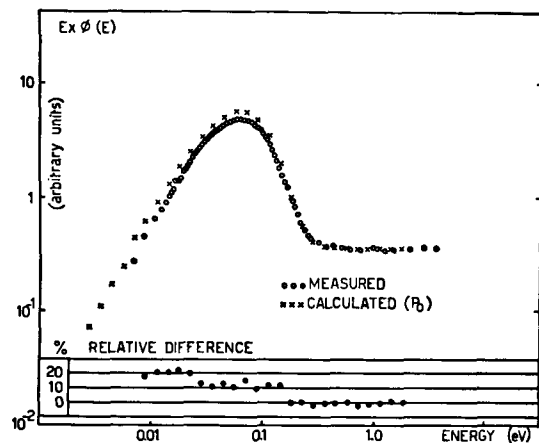


Fig. 3: Measured neutron spectrum in C_6H_6 compared to calculation using P_0 approximation

benzene from Gläser [13], specially using a frequency spectrum obtained from Marsden and McMurry data [10].

For the neutron total cross section the agreement was also better than the previous results, for the case of the modified Sprevak's frequency spectrum [8]. For this work it was necessary to remeasure this cross section [2] due to the evidence that the accuracy of known data [14-17] was not suitable for a definitive comparison.

From these results was selected for this work a model based on the vibrational frequency spectrum from Sprevak, a rotational spectrum adjusted to reproduce the Gläser data and diffusion motion, instead of free translation, for the whole molecule.

Calculations

The distributed moderation source in one dimension was calculated by the NYR232 code [18], using the measured transverse distribution of epithermal neutrons. Group cross sections for 30 energy groups were obtained with GASKET, NYR190 [19] and NYR081 [20] codes. The transport theory calculations were performed by the NYR230 [21] code in 30 spatial intervals and S_0 and P_0 approximations. The results of the calculated spectra are shown in Figs. 2 and 3 together with the experimental data.

Discussion of results

About the central spectrum, Fig. 2, the transport calculation agrees with the measured spectrum within -3 and $+6\%$, thus it is satisfactory; but it is possible to see that for energies of 0.009 and 0.0072 eV shows deviations to $+15\%$.

With respect to the leakage spectrum, Fig. 3, normalizing both theoretical and experimental values at epithermal region, the first one is 12% more thermalized, and for energies lower than 0.0225 eV the discrepancies are in the order of 20% or more. Also in this case appear anomalies at 0.009 and 0.0072 eV.

Conclusion

Taken into account that the experimental results were confirmed through new measurements, it is possible to conclude that calculations using group constants derived from the cited theoretical scheme in conjunction with a model based on the vibrational frequency spectrum from Sprevak, reproduce quite well a quasi-infinite-medium neutron spectra in benzene. But there are deviations not function on the position, at lower energies, that mean a selfscattering overestimated effect that must be studied.

From the leakage neutron spectrum results we conclude that anisotropic scattering must be used in the calculations and that more experimental information will be necessary in the region near the boundary for a better understanding of the discrepancies already shown. These works are at present under way.

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To the space dependence of reactivity noise in pressurized water reactors

Zur Raumabhängigkeit des Reaktivitätsrauschens in Druckwasserreaktoren

By D. Ziegenbein*

1. Introduction

Investigations of space-dependent effects on reactor dynamic perturbation measurements at pressurized water reactor (PWR) are reported in Ref. [1], the results are of interest for the space dependence of neutron noise, too. In [1] a determined reactivity perturbation is given on the reactor and the system response is measured. If the used outcore detector is arranged in different core heights then the measured signal is dependent on the detector position. This effect can be explained only by deviations of neutron flux from the behaviour according to the one-point model.

By using the adiabatic approximation it is possible to describe the measured effect by only one parameter [2] that can be estimated both by means of theoretical investigations [3] and experimentally [4]. In this way quantitative assertions on the space dependence of the global effect of neutron noise [5] are possible.

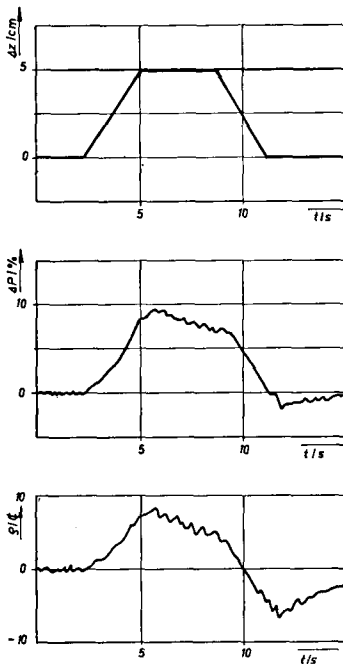


Fig. 1: Time dependence of control-rod position Δz , power ΔP and reactivity ρ

2. Space dependence of reactivity measurements

In the derivation of the one-point model of neutron kinetic the equation

$$\psi(r, t) = N(t) \phi^{(0)}(r) \quad (1)$$

is supposed. $\psi(r, t)$ describes the neutron flux density, $N(t)$ its time-dependent amplitude, $\phi^{(0)}(r)$ the stationary flux shape.

The investigations discussed in [1] show that in power reactors of WWER-440 type the neutron flux behaviour deviates from Eq. (1) also in the case of small reactivity perturbations.

If the reactor is disturbed by a reactivity perturbation according to Fig. 1, which is produced by the motion of a control rod bank then the measured normalized alternation of the detector signal would have to be independent on the detector position. The measurements do not show such a behaviour. It can be seen a distinct change of the measured signal if the ionization chamber is situated in different core heights.

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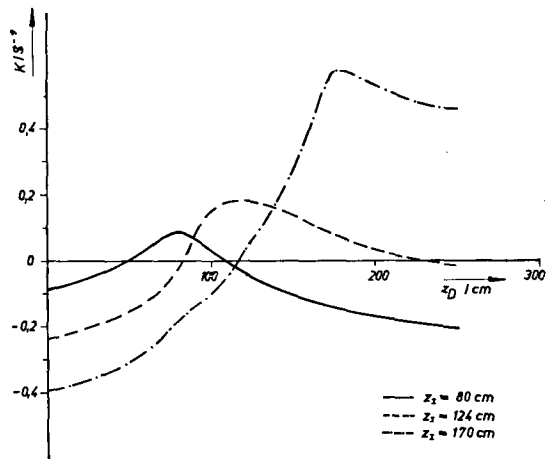


Fig. 2: Dependence of K on the detector z_D and perturbation positions z_I (zero power)

According to [3] the measured deviations from the one-point model behaviour can be described for the reactor without feedback (zero power) in good accuracy by the adiabatic approximation. In this case one obtains

$$\psi(r, t) = N(t) \phi^{(0)}(r) (1 + K(r; r_p) \Delta \rho(t)) \quad (2)$$

The additional term in Eq. (2) describes the flux shape alternation with the perturbation reactivity. In the plateau of the trapezoidal control rod motion on other flux shape exists than in the initial respectively final state. The flux shape alternation is described in the frame of the adiabatic approximation by Eq. (2). The factor K is space-dependent and also a function of the perturbation position r_p .

With the optimization procedure described in [3] it is possible to estimate K for the investigated perturbation from the obtained measured values. In [3] this was made with simulated values obtained by means of calculations with an one dimensional reactor dynamic code. The calculations are based on an axial geometry because the motion of a control bank above all produces a perturbation in the axial flux shape. The geometric data and the cross sections used in the code are typical for a PWR of WWER-440 type. In Fig. 2 the values of K are shown for different perturbation and detector positions. The maximum of K that is placed on the perturbation position or nearly to the reflector is in the order of 0.5. It strongly depends on the perturbation position; for positions far from the shape maximum $K > 1$.

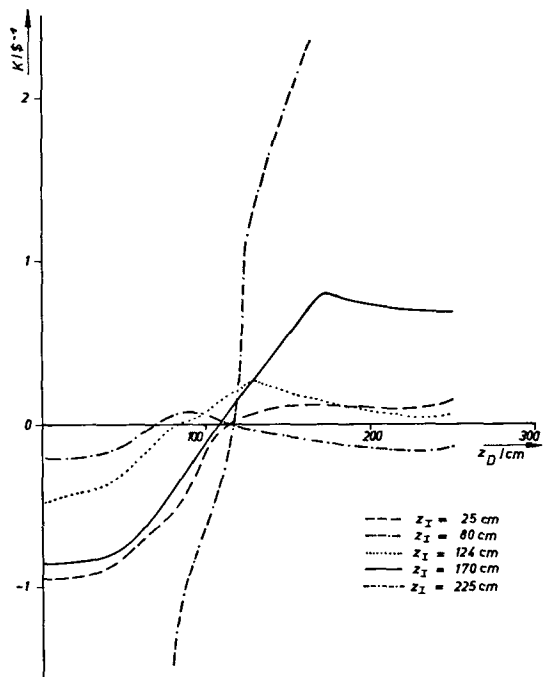


Fig. 3: Dependence of K on the detector z_D and perturbation positions z_I (full power)